

EVALPFC2-ICE2PCS01

300W PFC Evaluation Board with CCM PFC controller ICE2PCS01

Power Management & Supply



Never stop thinking.

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1 Content

The evaluation board described here is a 300W power factor correction (PFC) circuit with 85~265VAC universal input and 393VDC fixed output. Boost converter topology is employed in this board. The continuous conduction mode (CCM) PFC controller **ICE2PCS01** is employed in this board to achieve the unity power factor. The switching frequency is programmable by external resistor at one pin. There are various protection features incorporated to ensure safe system operation conditions. The device has a unique soft-start function which limits the start up inrush current thus reducing the stress on the boost diode. To improve the efficiency, the third generation **CoolMOS™** is used as the power switch due to its lowest area specific $R_{ds(on)}$. High voltage Silicon Carbide (SiC) Schottky diode **thinQ!™** is used as PFC boost diode. Because of its ideal reverse recovery behavior, SiC Schottky diode is extremely suitable for high frequency CCM PFC application.

2 Evaluation board





3 Technical specifications:

Input voltage	85VAC~265VAC
Input frequency	50Hz
Output voltage and current	393VDC, 0.75A
Output power	~ 300W
Efficiency	>90% at full load
Switching frequency	62.5kHz (with R8=76K)

4 Circuit Description

Line Input

The AC line input side comprises the input fuse F1 as over-current protection. The high frequency current ripple is filtered by R1, L1 and CX1. The choke L2, X2-capacitors CX1 and CX2 and Y1-capacitor CY1 and CY2 are used as radio interference suppressors. RT1 is placed in series to limit inrush current during each power on.

Power Stage – Boost Type PFC Converter

After the bridge rectifier BR1, there is a boost type PFC converter consisting of L3, Q1, D1 and C2. The third generation **CoolMOS™** is used as the power switch Q1. Due to its low $R_{ds(on)}$, the small heat sink can fulfill the dissipation requirement. SiC Schottky diode **thinQ!™** is used for D1. As SiC Schottky diode does not show a reverse recovery behavior, the stress on the MOSFET will be reduced due to very low current spike during turn on transient. Simultaneously higher reliability of the entire system can be achieved. However, due to the poor pulse current capability of SiC Schottky diode, a standard diode D2 is necessary to bypass the high inrush current during each power on transient. Output capacitor C2 provides energy buffering to reduce the output voltage ripple (100Hz) to the acceptable level.

PWM control of Boost Converter

The PWM control is realized by 8-Pin CCM PFC IC **ICE2PCS01**. Unlike the conventional PFC controller, **ICE2PCS01** does not need direct sine wave reference signal. The switching frequency is fixed and programmed by R8. There are two control loops in the circuit, voltage loop and current loop. The output voltage is sensed by the voltage divider of R5A, R5B, R6A and R6B and sent to internal error amplifier. The output of error amplifier is used to control current in the inner current loop. The compensation network C4, C5, R7 constitutes the external circuitry of the error amplifier. This circuitry allows the feedback to be matched to various load conditions, thereby providing stable control. In order not to make the response for 100Hz ripple, the voltage loop compensation is implemented with low bandwidth. The inner loop, current control loop, is implemented with average current mode strategy. The instant current is adjusted to be proportional to both of MOSFET off duty D_{OFF} and the error amplifier output voltage of voltage loop. The current is sensed by shunt resistors R2, R2A and R2B and fed into IC through R9. The current sense signal is averaged by an internal operating amplifier and then processed in the PWM generator which drives the gate drive. The averaging is realized by charging and discharging an external capacitor C7.

The IC supply is provided by external voltage source and filtered and buffered by C8 and C9. The IC output gate driver is a fast totem pole gate drive. It has an in-built cross conduction current protection and a Zener diode to protect the external transistor switch against undesirable over voltages. The gate drive resistor R4 is selected to limit and gate pulse current and drive MOSFET for fast switching.

5 Circuit Operation

Soft Start

When Vcc pin is higher than turn-on threshold, typical 11V, PFC is going to start. The unique soft start is integrated. Input current keeps sinusoidal and is increasing gradually until output voltage reaches



75% of rating. Because the peak current limit is not activated, the boost diode is not stressed with large diode duty cycle under high current.

Enhanced Dynamic Response

Due to inherent low bandwidth of PFC dynamic, in case of load jump, regulation circuit can not response fast enough and it will lead to large output voltage overshoot or drop. To solve this problem in PFC application, enhance dynamic response is implemented in the IC. Whenever output voltage exceeds by $\pm 5\%$, it will bypass the slow compensation operating amplifier and act on the nonlinear gain block to affect the duty cycle directly. The output voltage can be recovered in a short time.

Protection Features

a. Open loop protection (OLP) / Mains under voltage protection

The open loop protection is available for this IC to safe-guard the output. Whenever V_{SENSE} voltage falls below 0.6V, or equivalently V_{OUT} falls below 20% of its rated value, it indicates an open loop condition (i.e. VSENSE pin not connected). In this case, most of the blocks within the IC will be shutdown. It is implemented using a comparator with a threshold of 0.6V. Insufficient input voltage V_{IN} will also trigger this protection.

b. Output over-voltage protection

Output over-voltage protection is also available by the same integrated blocks of enhanced dynamic response. Whenever V_{OUT} exceeds the rated value by 5%, the over-voltage protection OVP is active. This is implemented by sensing the voltage at pin V_{SENSE} with respect to a reference voltage of 3.15V. A V_{SENSE} voltage higher than 3.15V will immediately reduce the output duty cycle even down to zero, bypassing the normal voltage loop control. This results in a lower input power and the output voltage V_{OUT} is reduced.

c. Soft over current control (SOC) and peak current limit

When the amplitude of current sense voltage reaches 0.68V, Soft Over Current Control (SOC) is activated. This is a soft control does not directly switch off the gate drive but acts on the internal blocks to result in a reduced PWM duty cycle.

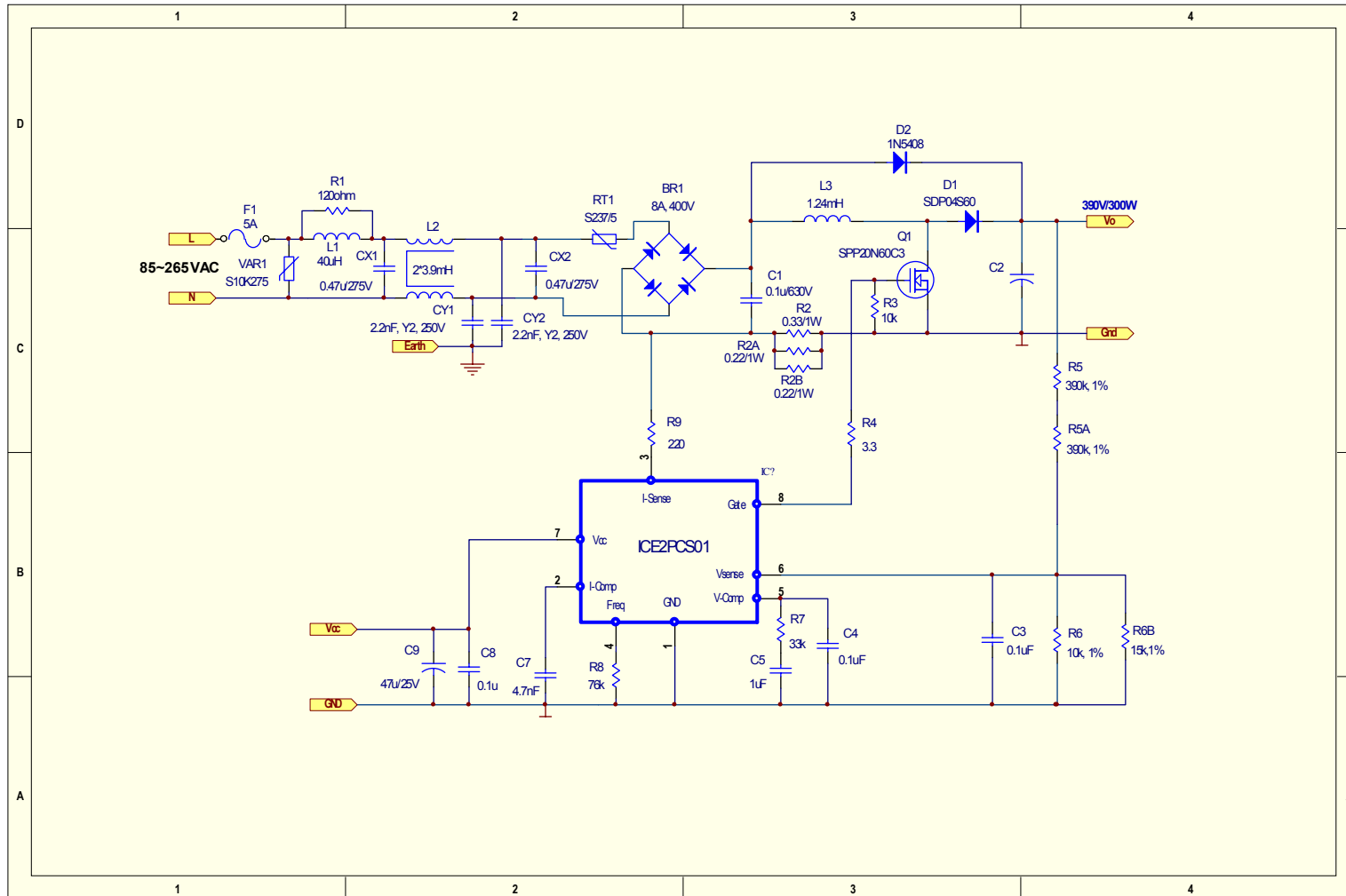
The IC also provides a cycle by cycle peak current limitation (PCL). It is active when the voltage at current sense voltage reaches -1.04V. The gate output is immediately off after 300ns blanking time.

d. IC supply under voltage lock out

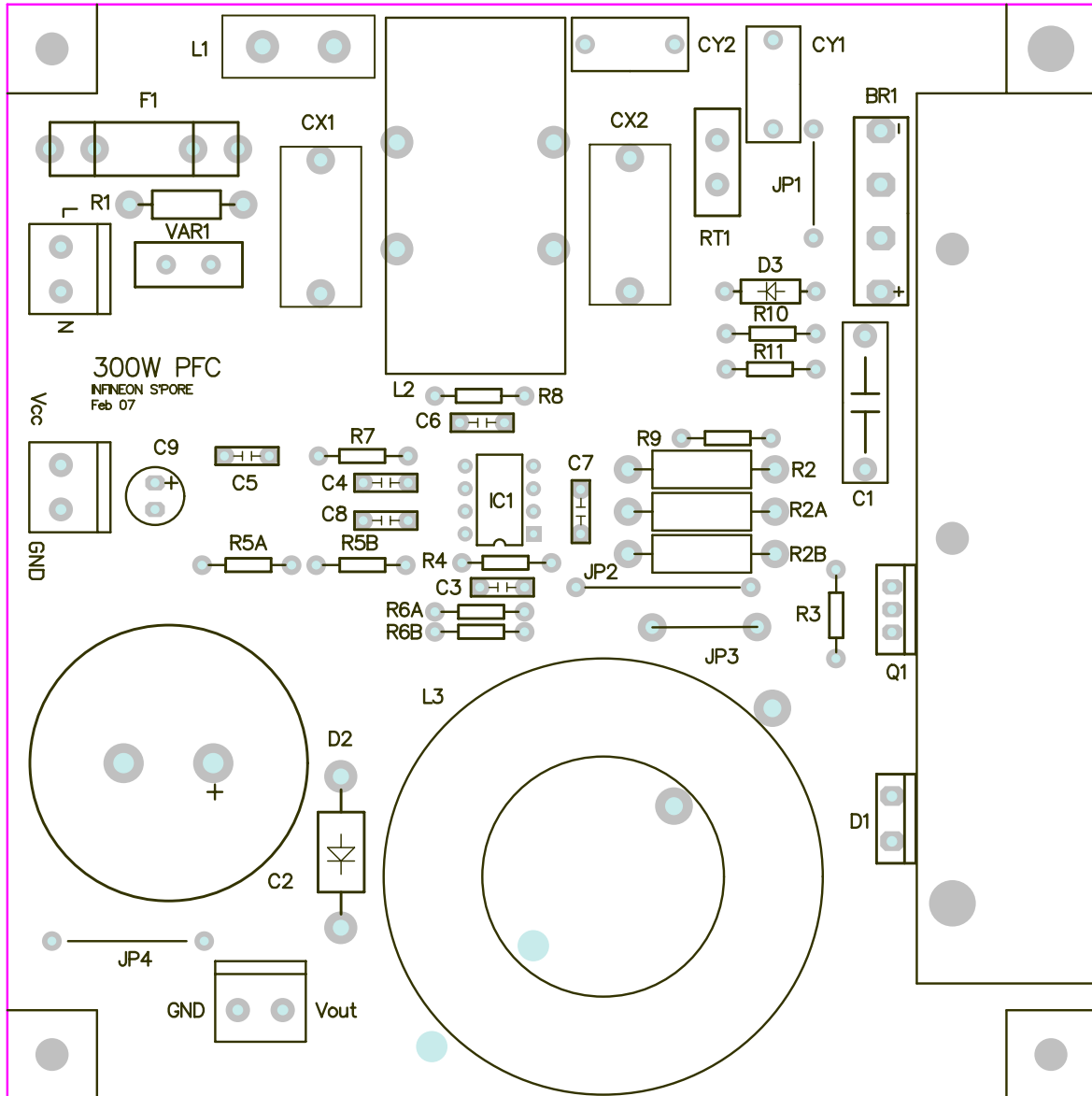
When VCC voltage is below the under voltage lockout threshold V_{CCUVLO} , typical 11V, IC is off the gate drive is internally pull low to maintain the off state. The current consumption is down to 200uA only.



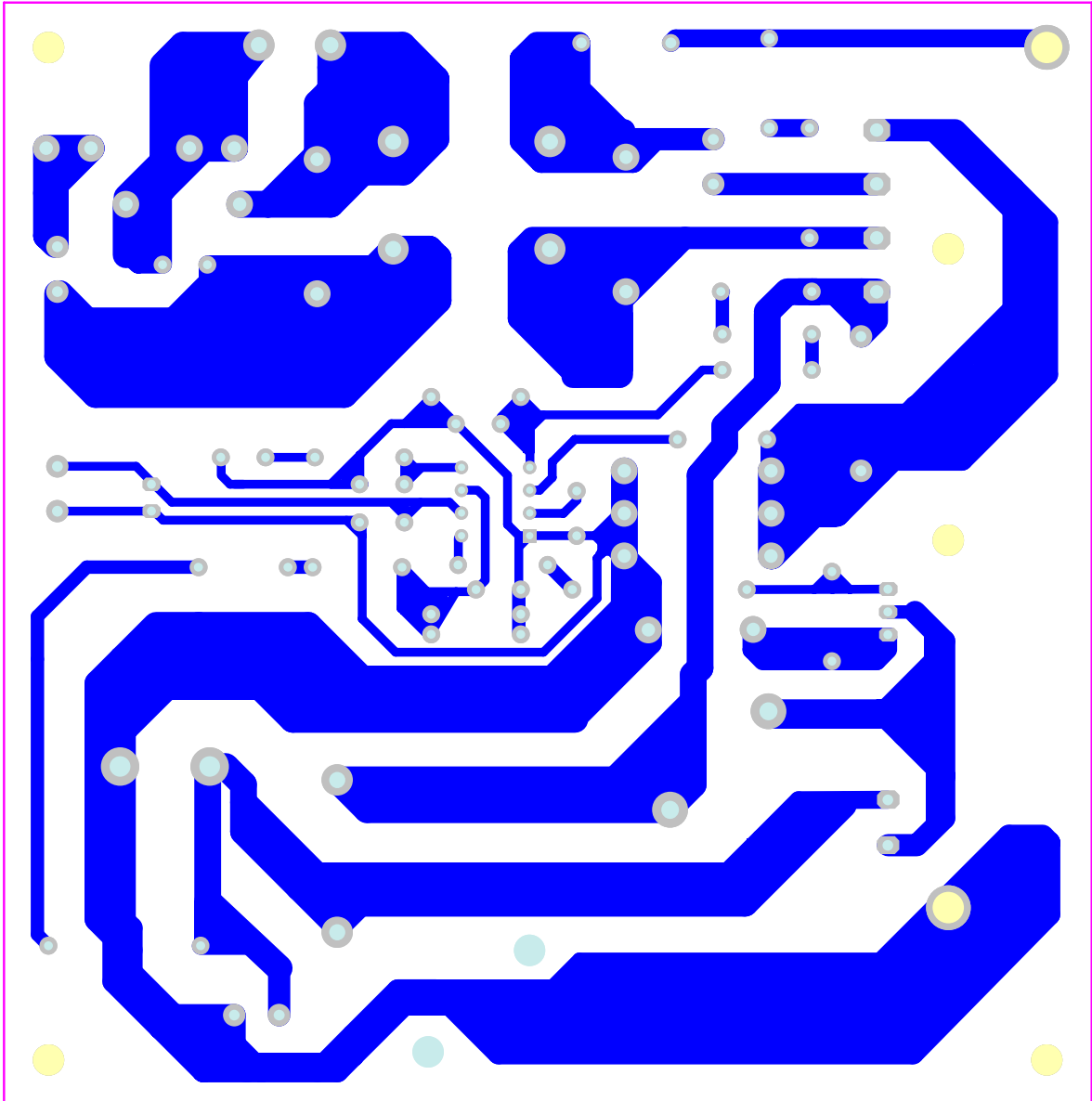
6 Circuit Diagram



7 PCB layout top layer



8 PCB layout Bottom:





9 Component List:

Designator	Part Type	Description	Manufacturer / Part No.
BR1	8A, 400V	Bridge Rectifier	Vishay / KBU8G
C1	0.1uF/630V	Ceramic Cap	Epcos / B32652A6104J
C2	220uF/450V	Electrolytic Cap	Epcos / B43304C5227M
C3	0.1uF/50V	Ceramic Cap	Murata / RPER71H104K2K1A03B
C4	0.1uF/50V	Ceramic Cap	Murata / RPER71H104K2K1A03B
C5	1uF/50V	Ceramic Cap	
C7	4.7nF/50V	Ceramic Cap	
C8	0.1uF/50V	Ceramic Cap	Murata / RPER71H104K2K1A03B
C9	47uF/25V	Electrolytic Cap	
CX1	0.47uF, X1, 305V	Ceramic Cap	Epcos / B32922C3474M
CX2	0.47uF, X1, 305V	Ceramic Cap	Epcos / B32922C3474M
CY1	2.2nF, Y2, 250V	Ceramic Cap	Epcos / B81123C1222M000
CY2	2.2nF, Y2, 250V	Ceramic Cap	Epcos / B81123C1222M000
		Connector	
D1	SDT04S60	Diode	
D2	1N5408	Diode	Vishay / 1N5408
F1	5A	Fuse	
		Fuse Holder	
IC1	ICE2PCS01		Infineon
JP1	12.5mm, Φ 0.7mm	Jumper	
JP2	20mm, Φ 0.7mm	Jumper	
JP3	12mm, Φ 1.2mm	Jumper	
JP4	17.5mm, Φ 0.7mm	Jumper	
L1*	Shorted		
L2	2*3.9mH	CM Choke	Epcos / B82725J2602N20
L3	1.24mH	Choke	
Q1	SPP20N60C3	Power MOSFET	Infineon
		Heat Sink	
		TO220 Clip	
		TO247 Clip	
		TO220 Isolation Pad	
		3mm Screw	
R2	0.33/1W, 5%	Metal Film Resistor	
R2A	0.22/1W, 5%	Metal Film Resistor	
R2B	0.22/1W, 5%	Metal Film Resistor	
R3	10k/0.25W, 5%	Carbon Film Resistor	
R4	3.3/0.25W, 5%	Carbon Film Resistor	
R5A	390k/0.25W, 1%	Carbon Film Resistor	
R5B	390k/0.25W, 1%	Carbon Film Resistor	
R6A	10k/0.25W, 1%	Carbon Film Resistor	
R6B	15k/0.25W, 1%	Carbon Film Resistor	
R7	33k/0.25W, 5%	Carbon Film Resistor	
R8	75k/0.25W, 1%	Carbon Film Resistor	
R9	220/0.25W, 5%	Carbon Film Resistor	
RT1	S237/5	NTC Thermistor	Epcos / B57237S509M
VAR1	S10K275	Varistor	Epcos / B72210S271K101



10 Boost Choke Layout

Core: CS468125 toriod

Turns: 83

Wire: 1 x Φ 1.0mm, AWG19

Inductance: L=1.24mH

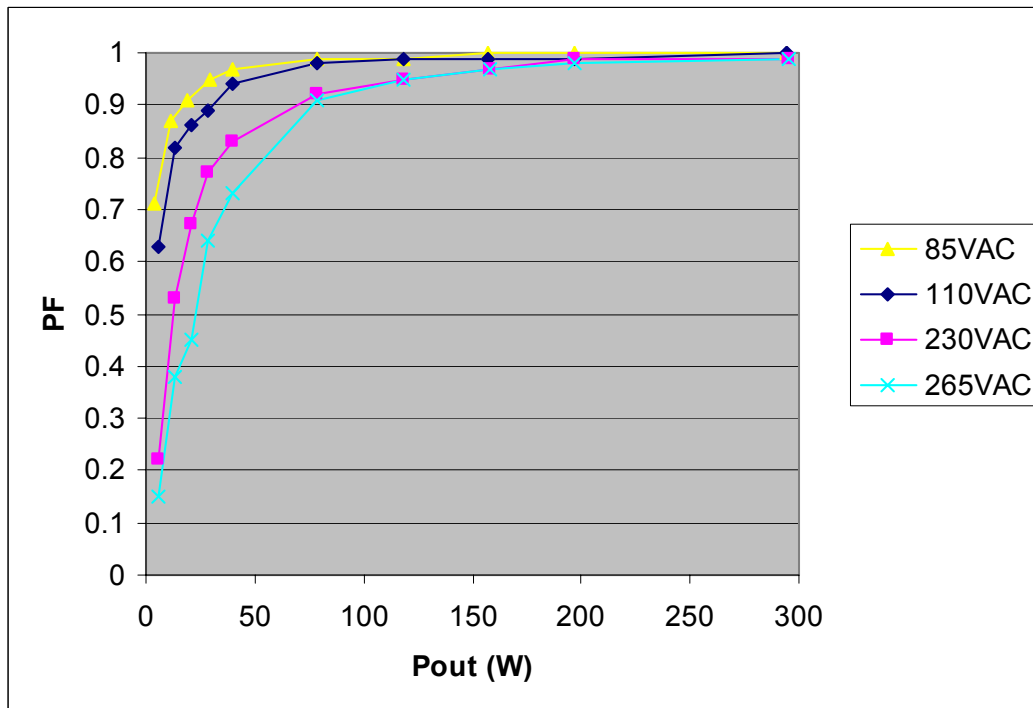
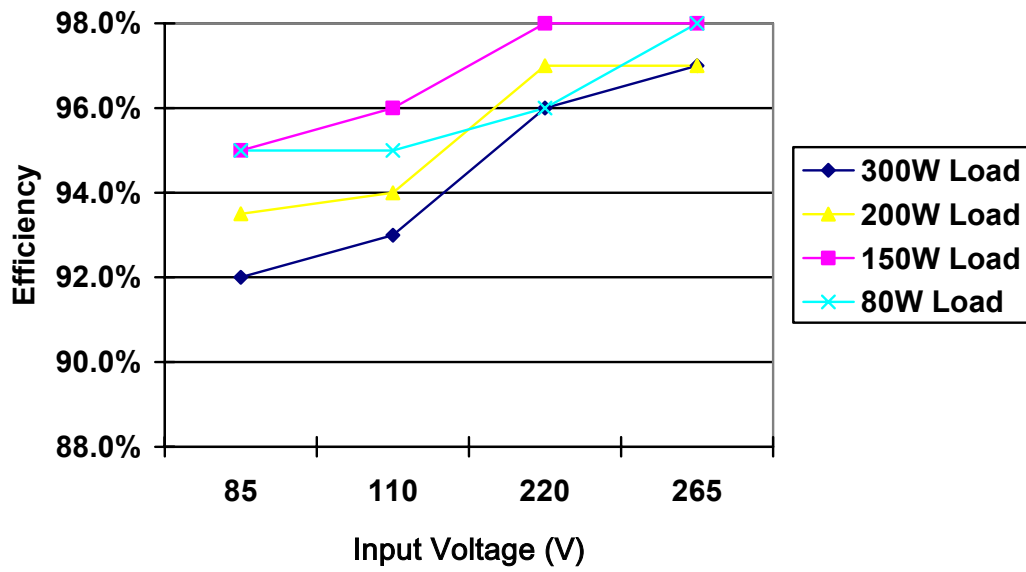
11 Test report

11.1 Load test (table and figure):

Vin (VAC)	Pin (W)	Iin (A)	Vout (V)	Iout (A)	Pout (W)	efficiency	PF
85	320	3.8	393	0.75	294.75	92%	1
	211	2.51	393	0.5	196.5	93%	1
	165	1.96	393	0.4	157.2	95%	1
	124	1.47	393	0.3	117.9	95%	0.99
	83	0.99	393	0.2	78.6	95%	0.99
	43	0.52	394	0.1	39.4	92%	0.97
	31	0.39	394	0.075	29.55	95%	0.95
	20.3	0.26	395	0.049	19.355	95%	0.91
	12.2	0.17	396	0.029	11.484	94%	0.87
110	4.2	0.07	396	0.01	3.96	94%	0.71
	316	2.9	393	0.75	294.75	93%	1
	208	1.91	393	0.5	196.5	94%	0.99
	163	1.5	393	0.4	157.2	96%	0.99
	123	1.13	393	0.3	117.9	96%	0.99
	83	0.77	393	0.2	78.6	95%	0.98
	42.3	0.4	393	0.1	39.3	93%	0.94
	30	0.29	394	0.0718	28.2892	94%	0.89
	22	0.22	394	0.0525	20.685	94%	0.86
220	14.2	0.15	394	0.034	13.396	94%	0.82
	6.2	0.076	394	0.014	5.516	89%	0.63
	307	1.4	394	0.75	295.5	96%	0.99
	204	1	394	0.5	197	97%	0.99
	161	0.8	394	0.4	157.6	98%	0.97
	120	0.63	394	0.3	118.2	99%	0.95
	82	0.45	394	0.2	78.8	96%	0.92
	41	0.29	394	0.1	39.4	96%	0.83
	29.5	0.16	395	0.072	28.44	96%	0.77
265	21.7	0.133	395	0.053	20.935	96%	0.67
	14	0.1	395	0.033	13.035	93%	0.53
	6	0.093	395	0.014	5.53	92%	0.22
	305	1.2	394	0.75	295.5	97%	0.99
	203	0.79	394	0.5	197	97%	0.98
	161	0.63	394	0.4	157.6	98%	0.97
265	120	0.48	395	0.3	118.5	99%	0.95
	81	0.34	395	0.2	79	98%	0.91
	41	0.21	395	0.1	39.5	96%	0.73

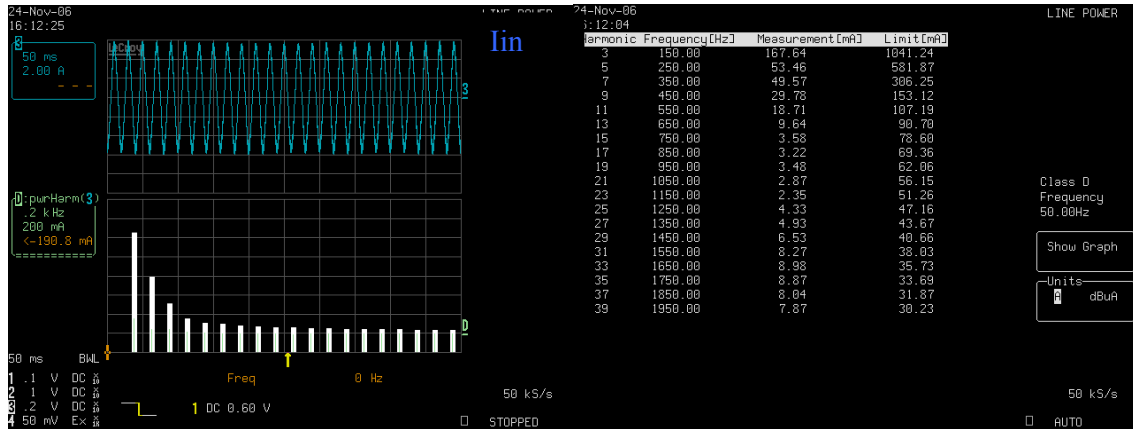


29.5	0.17	395	0.072	28.44	96%	0.64
21.7	0.16	395	0.053	20.935	96%	0.45
13.8	0.15	395	0.033	13.035	94%	0.38
5.83	0.1	395	0.014	5.53	95%	0.15

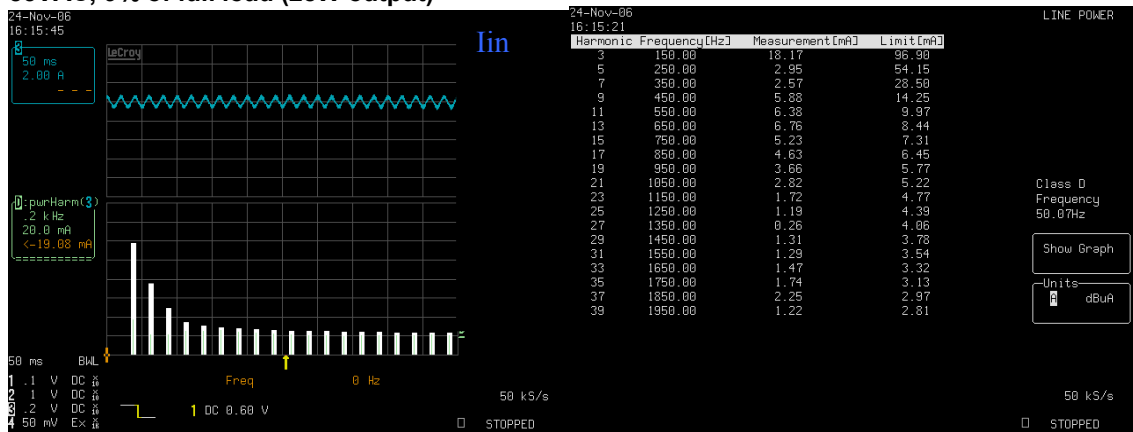


11.2 Harmonic test according to EN61000-3-2 Class D requirement

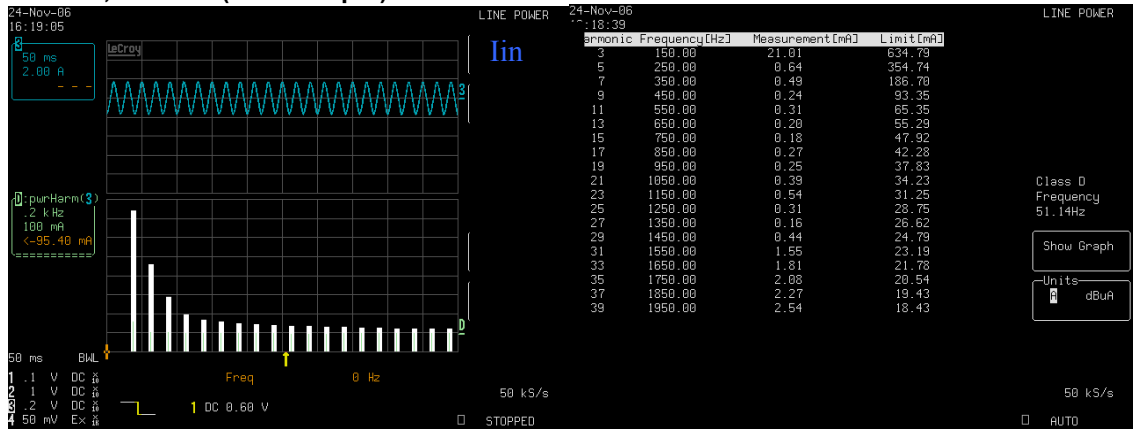
85VAC, full load (300W output)



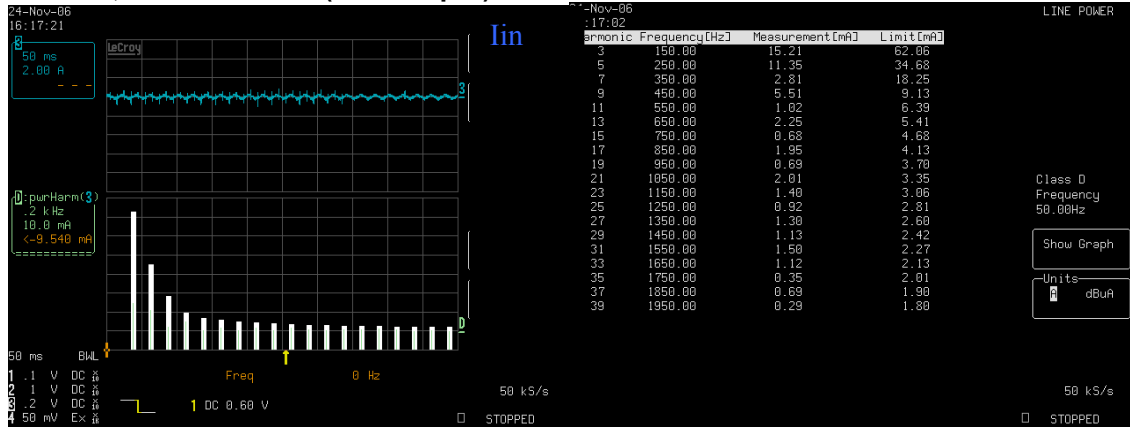
85VAC, 9% of full load (28W output)



265VAC, full load (300W output)

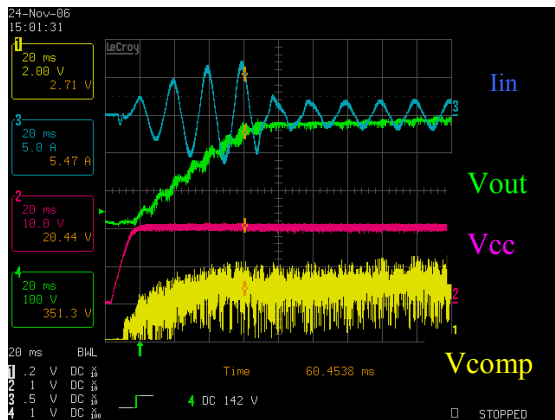


265VAC, 9% of full load (28W output)

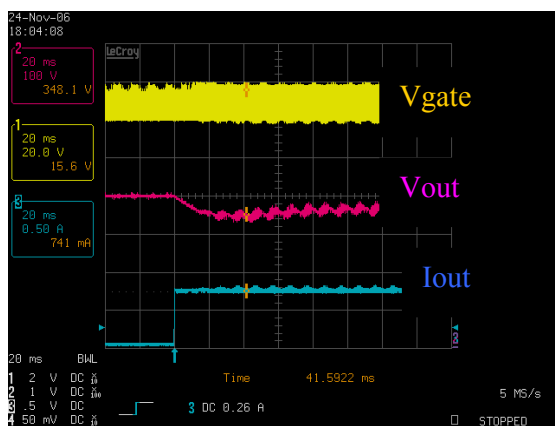


11.3 Waveforms (soft start, load jump, open loop)

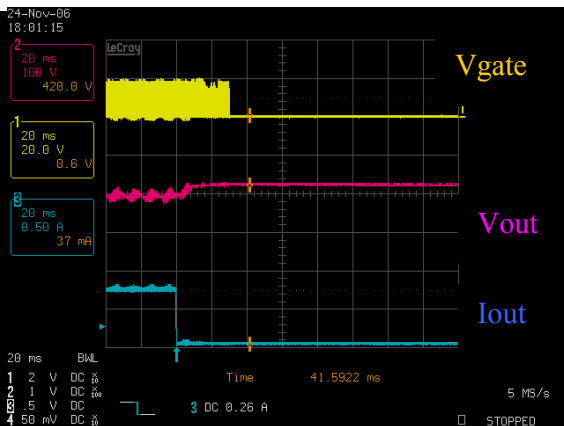
Soft start, test at 85VAC, Iout=0.2A



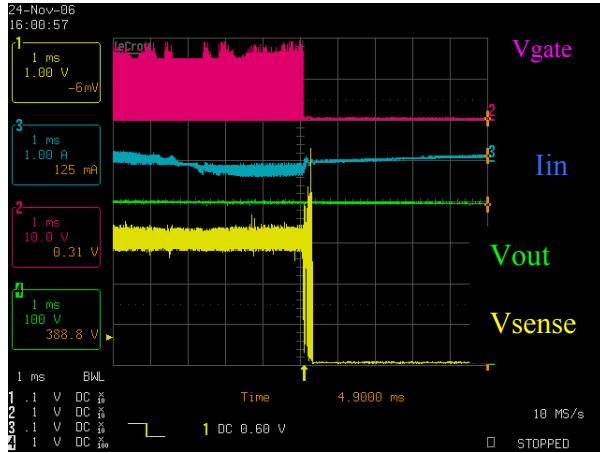
Load jump test at 85VAC, Iout from 0A to 0.75A



Load jump test at 85VAC, Iout from 0.75A to 0A



Open loop test at 265VAC, $I_{out}=0.1A$



12 References: